# SENSORS AND TRANSDUCERS

A transducer is a device that converts one form of onergy or physical quantity into another, in accordance with some defined relationship. Where a transducer is the suraing element, which responds directly to the physical quantity to be measured and this forms part of an isotromonation or control system, then the transducer is obtained on a sensor.

In data acquicition systems, transducers some physical phenomena and provide electrical signals that the system can accept. For example, thermocouples, no orive temperature denotes (RTD's), thermistore, and IC samore convert temperature into an analysis of orlarge signal, while flow transducers produce digital pulse trains whose frequency depends on the speed of flow.

Two defined categories of transducer exist.

- Active transducers convert non-electrical energy into an electrical energy signal. They do not require external excitation to operate. Thermocouples are an example of an active transducer.
- Passive transforms change an electrical network value, such as resistance, inductance or capacitance, according to changes in the physical quantity being massened. Strain gauges (resistive change to ensus) and LXDTV (inductance change to displacement) are two examples to this. To be able to detect such changes, possive division require external societarion.

## Transducer Characteristics

Transducere are classified according to the physical quantity they measure (a.g. temperature, force erc). Boyout the obvious selection of the type of transducer required to measure a particular physical quantity and any cost considerations, the characteristics which are most important in determining a transducers applicability for a given application are as follows:

- Accuracy
- Souskivky
- Reputability
- Range

### Accuracy

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### Sensitivity

Similarity is defined as the amount of change in the output signal from a transducer to a specified change in the input variable being measured. Highly sensitive devices, such as thermistere, may change minimare by as much as 5% per 0C, while devices with irow sensitivity, such as thermocouples, may produce an output visings that changes by only 5 mV per 0C.

#### Reveatability

If two or more measurements are made of a precess variable at the identical state, a translocar's repeatability indicates how close the repeated measurements will be. The ability to generate almost identical compart responses to the same physical input throughout its working Ho is an indication of the translateurs reliables and is sumply indicat to the cost of the translateur.

#### Range

A transford is usually construed to operate within a specified maps. The maps is defined as the minimum and maximum measurable values of a process variable burness which the defined limits of all other equicided transforder. It is an additional, accuracy exit are and. A humocouple, for example, could will work omida in specified operating maps of 0 CC to 500 CC, however its susticity conside this maps maps how small to produce accurate or specified measurements.

Them are several variables that affect the accuracy, unwittivity and repeatability of the measurements being made:

- In the process of measuring a physical quantity, the transducer disturbs the system being monitored. As an example, a temperature measuring transducer lowers the temperature of the system being monitored, while energy is used to hast its own mass.
- Transducers are responsive to unwanted noise in the same way that a record players magnetic carridge is soluble to the abreasting magnetic field of the mains transformer (giving rise to mains hum).
- Some transduces are subject to excitation signals that after its response to the input physical quantity being measured. As an example, an RTD's excitation current can result in self-baseing of the device, theory changing its restaurce.

## Resistance Temperature Detectors (RTD's) Characteristics of RTD's

Resistance nonpentativ detectors (RTD's) are tompentativ sources generally studie from a pairs (or lightly dipod) metal whose resistance increases with increasing temperature (politive resistance temperature coefficient).

Most BTD devices are other wire vessel or near BTm. Wave vessel devices are seemingly a length of wire vessel are a second or and howed in a presencior down. We fill for BTD's an device in which the restrict element is hild down on a commissi substrate are a graph multilly task a few micrometers thus, The notenance is provide yourself by they writeming of the must multille. Task a few micrometers thus, increased an element work of the second second

The non-papelar RTD is the placement the PT100 (DSA 13700 Standard), with a seminal resistance of 100 W = 0.1 W = 0.0 K = 0.0 Cminum is usually used for RTD is because of a stability our a value of the stability of the stab

## Linearity of RTD's

In comparison to other transportants meaning devices such as thermocouples and thermitexts, the change is needings of an 2014 with respect to transportant is relatively linear out a valia transportante range, exhibiting only a vory digite server over the veeding transportants range. Abhong is a such as a such as the information of the server of the set of the server of the set of the server of the set of the server distribution of the set of the s

Alpha (a) = 
$$\frac{R_{100} - R_0}{100 \sqrt{R}} = \Omega / \Omega / C$$

where:

- R<sub>c</sub> = Resistance at 0°C
- R., = Resistance at 100°C

This represents the change in the resistance of the RTD from 0°C to 100°C, divided by the resistance at 0°C, divided by 100°C.

From the expression of alpha (st) it is easily derived that the resistance R, of an RTD, at temperature T can be found from the expression:

 $R_{i} \approx R_{i} (1+\alpha T)$ 

where

R<sub>1</sub> = novietance at 0°C

For example, the PT100 (DIN 43760 Standard), with nominal resistance of

100  $\Omega$  = 0.1  $\Omega$  at 0 °C has an alpha (ii) of 0.00785  $\Omega$  /  $\Omega$  / °C.

Measurement Circuits and Considerations for RTD's

Since the RTD is a passive resistive divice, it requires an excitation current to produce a measurable voltage across it. Figure 1 shows a two-wire RTD excited by a constant current source, I<sub>40</sub> and connected to a measuring divice.



Any molenance, R., in the lead wires hereness the measuring device and the RTD will cause a voltage deep on the leade equal to (R, x L), white. The voltage deep on the wire leade will add to the voltage deep across the RTD, and depending on the value of the dwire molenance compared to the resistance of the RTD, may result in a circulticast error in the calculated trememate.

Consider an example where the lead meistance of each wire is  $0.5 \ \Omega$ . For a 100 to RTD with an alpha (tt) of  $0.385 \ \Omega^{\prime}$ C, the lead meistance corresponds to a temperature error of  $2.6^{\circ}$ C (1.02/0.385 $\Omega^{\prime}$ C).

This indicates that if voltage measurements are made using the same two wires which carry the excitation current, the restinance of the RTD must be large enough, or the land wire restinances small enough, that voltage deeps due to the land wire restrances are negligible. This is usually true where the lands are no larger than a law (c) means to for a 100 D RTD.

#### Four-Wire RTD Measurement

A better method of excitation and measurement, especially when the wire lead lengths are greater than a few meters in length, is the four-wire RTD configuration shown in Figure 2.



#### Figure 2 Four-Wey KTD Measurement

RTDs are cosmooly packaged with four (6) inde, two current leads to precide the excitation current for the derice, and two voltage leads for measurement or the voltaged evolvaged. This configuration eliminature the voltage deeps caused by excitation current through the lead resistances ( $\mathbf{R}_{ii}$  and  $\mathbf{R}_{ii}$ ). Since negligible current flows in the voltage land resistances ( $\mathbf{R}_{ii}$  and  $\mathbf{R}_{iii}$ ) only the voltage deep across the resistance RT of the RTD in meaned.

## Three-Wire RTD Measurement

A reduction in cost is possible with the elimination of one of the wire leads. In the three-wire configuration shown in Figure 3, only one lead RL1 adds an error to the RTD voltage measured.



Figure 3. Three Wey #TD Measurement

## Self-Heating

Another consequence of current excitation of the RTD; is the possible effect that internal basing of the device may have on the accuracy of the actual temperature measurements being made. The degree of self heating depends on the medium is which the RTD is being used, and is typically specified as the rise in temperature for each teW of power dissipated for a given medium (i.e. still all s).

For a PT100 RED device, the sub-basing coefficient is  $0.2^{\circ}CheW$  is still as, although this will vary depending on the construction of the RED baseling and its thermal properties. With an architelon current of 0.75mA the power to be dissipated by the device is  $85 \text{ gW} [0.758110^{\circ} \times 100]$  consequending to arise in the temperature of the device to suff-basing of  $0.011^{\circ}C$  ( $86 \text{ W} \times 0.2$ ).

Inaccuracies in the temperature measurement due to self-heating problems, can be eready reduced by:

- Minimizing the excitation power
- Exciting the RTD's only when a measurement is taken
- Calibratine out meady mane errors