

# Cement And Water Saving With Water Reducers

By

Er. Kaushal Kishore ,

Materials Engineer, Roorkee

In India 0.93 kg of CO<sub>2</sub> is emitted in the production of one kg of cement. In the financial year 2009-10 India produces 200 million tonnes of cement. In the production of this cement 186 million tonnes of CO<sub>2</sub> was emitted in the atmosphere during financial year of 2009-10. The availability of water in India per person per year in 1950 was 5177 cu.m. In the year 2009 it is reduces to 1700 cu.m.

If 50 million tonnes cement in making concrete uses water reducers 7500000 tonnes of cement can be saved. 3750000 kl of potable water will be saved and the saving of Rs. 3300 crores per year to construction industry. This amount is worked out after adjusting the cost of water reducers. Less cement used means less cement required to be produce by the cement factories resulting 6975000 tonnes of CO<sub>2</sub> will be prevented to be emitted to the atmosphere. These are worked out with an average saving of 15% cement and 15% water. CO<sub>2</sub> emission is word problem, but for India in addition to CO<sub>2</sub> it has problems of Air, Water, Soil, Food and Noise pollutions. Less densily populated countries may cope with these problems but for India it is of the top concern. The population figures of 2009 is, India 350 person per sq.km, China 132 person per sq.km and USA only 34 person per sq.km. The figures of 2006 CO<sub>2</sub> emissions are USA 658.60 tonnes per sq.km, China 611.76 tonnes per sq.km and India 459.35 tonnes per sq.km. Every one should contribute his or her efforts to save the environment from pollution. Those involve in the construction activities can contribute their share by proper design of concrete Mixes. This is best illustrated by the following examples.

## MIX DESIGN DETAILS

1	Grad of Concrete	:	M-30
2	Cement	:	Three mixes are to be designed
			<b>MIX-A</b> With PPC (Flyash based) conforming to IS:1489-part-I-1991. 7 days strength 38.5 N/mm <sup>2</sup> . Specific Gravity : 3.00

			<b>MIX-B</b> With OPC-43- Grade conforming to IS: 8112-1989. 7 days strength 40.7 n/mm <sup>2</sup> . Specific Gravity : 3.15
			<b>MIX-C</b> With OPC of Mix-B and Fly ash conforming to IS:3812 (Part-I)-2003 Specific Gravity : 2.25
			<b>Note:</b> Requirements of all the three mixes are the same. Fine Aggregate, Coarse Aggregate and normal Super plasticizer are the same for all the three mixes.
3	Fly ash replacement	:	30% Fly ash is required to be replaced with the total cementitious materials.
4	Maximum nominal size of aggregates	:	20 mm Crushed aggregate
5	Fine aggregate	:	River sand of Zone-II as per IS:383-1970
6	Minimum cement content	:	320 kg/m <sup>3</sup> including Fly ash
7	Maximum free W/C Ratio	:	0.45
8	Workability	:	50 mm slump
9	Exposure condition	:	Severe for RCC work
10	Method of placing	:	Site mixing
11	Degree of supervision	:	Good
12	Maximum of cement content (Fly ash not included)	:	450 kg/m <sup>3</sup>
13	Chemical admixture	:	Super plasticizer conforming to IS:9103-1999. With the given requirements and materials, the manufacturer of Normal Super plasticizer recommends dosages of 17 gm per kg of OPC, which will reduce 24% of water without loss of workability. For fly ash included cement dosages will be required to be adjusted by experience/ trials.

### TEST DATA FOR MATERIALS

1. The grading of fine aggregate, 10 & 20 mm aggregates are as given in Table. 1. Fine aggregate is of zone-II as per IS:383-1970. 10 and 20 mm crushed aggregate grading are single sized as per IS: 383-1970.
2. Properties of aggregates

Tests	Fine aggregate	10 mm aggregate	40 mm aggregate
Specific Gravity	2.65	2.65	2.65
Water Absorption%	0.8	0.5	0.5

3. Target strength for all A, B and C mixes

$$f_{ck} = f_{ck} + 1.65 \times S$$

$$30 + 1.65 \times 5$$

$$= 38.3 \text{ N/mm}^2 \text{ at 28 days age}$$

4. For Mix A and B free W/C ratio with crushed aggregate and required target strength of 38.3 N/mm<sup>2</sup> at 28 days from Fig. 1 Curve D found to be 0.45. Taking into the consideration of water in admixture, let it be 0.44. This is lower than specified maximum W/C ratio value of 0.45.

Note: In absence of cement strength, but cement conforming to IS Codes, assume from Fig. 1 and Fig. 2.

Curve A and B for OPC 33 Grade

Curve C and D for OPC 43 Grade

Curve E and F for OPC 53 Grade

Take curves C and D for PPC, as PPC is being manufactured in minimum of 43 Grade of strength.

5. Other data's: The Mixes are to be designed on the basis of saturated and surface dry aggregates. At the time of concreting, moisture content of site aggregates are to be determine. If it carries surface moisture this is to be deducted from the mixing water and if it is dry add in mixing water the quantity of water required for absorption. The weight of aggregates are also adjusted accordingly.

### **DESIGN OF MIX-A WITH PPC**

a) Free W/C ratio for the target strength of 38.3 N/mm<sup>2</sup> as worked out is 0.44.

b) Free water for 50 mm slump from Table 2 for 20 mm maximum size of aggregate.

$$2/3 \times 180 + 1/3 \times 210 = 190 \text{ kg/mm}^3$$

From trials it is found that Normal Super plasticizer at a dosages of 20gm/kg of cement may reduce 24% water without loss of workability Then water =  $190 - (190 \times 0.24) = 144.4$  kg/m<sup>3</sup>

for trials say 145 kg/m<sup>3</sup>

c) PPC =  $145/0.44 = 329.5$  kg/m<sup>3</sup>

Say 330 kg/m<sup>3</sup>. This is higher than minimum requirement of 320 kg/m<sup>3</sup>

d) Formula for calculation of fresh concrete weight in kg/m<sup>3</sup>

$$U_M = 10 \times G_a(100 - A) + C_M (1 - G_a / G_c) - W_M (G_a - 1)$$

Where,

$U_M$  = Wight of fresh concrete kg/m<sup>3</sup>

$G_a$  = Weighted average specific gravity of combined fine and coarse aggregate bulk, SSD

$G_c$  = Specific gravity of cement. Determine actual value, in absence assume 3.15 for OPC and 3.00 for PPC (Fly ash based)

$A$  = Air content, percent. Assume entrapped air 1% for 40 mm maximum size of aggregate, 1.5% for 20 mm maximum size of aggregate and 2.5% for 10mm maximum size of aggregate. There are always entrapped air in concrete. Therefore ignoring entrapped air value as NIL will lead the calculation of higher value of density.

$W_M$  = Mixing water required in kg/m<sup>3</sup>

$C_M$  = Cement required, kg/m<sup>3</sup>

Note:- The exact density may be obtained by filling and fully compacting constant volume suitable metal container from the trial batches of calculated design mixes. The mix be altered with the actual obtained density of the mix.

$$\begin{aligned} U_M &= 10 \times G_a (100 - A) + C_M (1 - G_a / G_c) - W_M (G_a - 1) \\ &= 10 \times 2.65 (100 - 1.5) + 330(1 - 2.65/3.00) - 145 (2.65 - 1) \\ &2409.6 \text{ kg/m}^3 \end{aligned}$$

Say 2410 kg/m<sup>3</sup>

e) aggregates =  $2410 - 330 - 145 = 1935$  kg/m<sup>3</sup>

f) Fine aggregate = From Table 3 for zone-II Fine aggregate and 20 mm maximum size of aggregate, W/C ratio = 0.44, 50 mm slump found to be 34%.

$$\text{Fine aggregate} = 1935 \times 0.34 = 658 \text{ kg/m}^3$$

$$\text{Coarse aggregate} = 1935 - 658 = 1277 \text{ kg/m}^3$$

10 and 20 mm aggregate are single sized as per IS: 383-1970. Let them be combined in the ratio of 1.2:1.8 to get 20 mm graded aggregate as per IS: 383-1970

$$10 \text{ mm aggregate} = 510 \text{ kg/m}^3$$

$$20 \text{ mm aggregate} = 767 \text{ kg/m}^3$$

g) Thus for M-30 Grade of concrete quantity of materials per cu.m. of concrete on the basis of saturated and surface dry aggregates:

$$\text{Water} = 145 \text{ kg/m}^3$$

$$\text{PPC} = 330 \text{ kg/m}^3$$

$$\text{Fine Aggregate (sand)} = 658 \text{ kg/m}^3$$

$$10 \text{ mm Aggregate} = 510 \text{ kg/m}^3$$

$$20 \text{ mm Aggregate} = 767 \text{ kg/m}^3$$

$$\text{Normal Super Plasticizer} = 6.6 \text{ kg/m}^3$$

#### **MIX- B WITH OPC**

$$\text{a) Water} = 190 - (190 \times 0.24) = 144.4 \text{ kg/m}^3 \text{ say } 145 \text{ kg/m}^3$$

$$\text{b) OPC} = 145/0.44 = \text{say } 330 \text{ kg/m}^3$$

c) Density:

$$10 \times 2.65 (100 - 1.5) + 330 (1 - 2.65/3.15) - 145 (2.65 - 1) \\ = 2423.5 \text{ kg/m}^3 \text{ say } 2425 \text{ kg/m}^3$$

$$\text{d) Total Aggregates} = 2425 - 145 - 330 = 1950 \text{ kg/m}^3$$

$$\text{Fine Aggregate} = 1950 \times 0.34 = \text{say } 663 \text{ kg/m}^3$$

$$\text{Coarse aggregate} = 1950 - 663 = 1287 \text{ kg/m}^3$$

$$10 \text{ mm Aggregate} = 1287 \times 1.2/3 = 515 \text{ kg/m}^3$$

$$20 \text{ mm Aggregate} = 1287 \times 1.8/3 = 772 \text{ kg/m}^3$$

e) Thus for M-30 Grade of concrete quantity of materials per cu.m of concrete on the basis of SSD aggregates are given below:

$$\text{Water} = 145 \text{ kg/m}^3$$

$$\text{OPC} = 330 \text{ kg/m}^3$$

$$\text{Fine Aggregate (sand)} = 663 \text{ kg/m}^3$$

$$10 \text{ mm Aggregate} = 515 \text{ kg/m}^3$$

20 mm Aggregate = 772 kg/m<sup>3</sup>

Normal Super Plasticizer = 5.610 kg/m<sup>3</sup>

### **MIX. C WITH OPC + FLYASH**

With the given set of materials increase in cementitious materials = 12%

Total cementitious materials = 330 x 1.12 = 370 kg/m<sup>3</sup>

<b>Materials</b>	<b>Weight (kg/m<sup>3</sup>)</b>	<b>Volume (m<sup>3</sup>)</b>
OPC = 370 x 0.70	259/3150	0.0822
Flyash = 370x 0.30	111/2250	0.0493
Free Water = 145 x 0.95	138/1000	0.138
Normal Super Plasticizer = 7.5kg	7.5/1150	0.0065
Air = 1.5%		0.015`
	<b>Total</b>	<b>0.291</b>
Total Aggregates = 1 – 0.291		0.709
		1.00
Coarse Aggregate	1287/2650	0.4857

Fine Aggregate = 0.709 – 0.4857 = 0.2233

= 0.2233 x 2650 = 592 kg

Note:-

1. Specific gravity of Normal Superplasticizer = 1.15
2. Addition of Flyash reduces 5% of water demand.

**M-30 Grade of concrete quantity of material per cu.m of concrete on the basis of saturated and surface dry aggregates of Mix 'A', 'B' and 'c' are given below:**

Materials	MIX. 'A' with PPC	Mix. 'B' with OPC	Mix. 'C' with OPC+Flyash
Water kg/m <sup>3</sup>	145	145	138
PPC kg/m <sup>3</sup>	330	—	—
OPC kg/m <sup>3</sup>	—	330	259
Flyash kg/m <sup>3</sup>	—	—	111
Fine Agg. kg/m <sup>3</sup>	658	663	592
10mm Agg. kg/m <sup>3</sup>	510	515	515
20 mm Agg. kg/m <sup>3</sup>	767	772	772
Normal Super-plasticizer kg/m <sup>3</sup>	6.6	5.61	7.5
W/Cementations ratio	0.44	0.44	0.373

Note:-

1. For exact W/C ratio the water in admixture should also be taken into account.
2. The W/C ratio of PPC and OPC is taken the same assuming that the strength properties of both are the same. If it is found that the PPC is giving the low strength then W/C ratio of PPC have to be reduce, which will increase the cement content. For getting early strength and in cold climate the W/C ratio of PPC shall also be required to be reduced.
3. PPC reduces 5% water demand. If this is found by trial then take reduce water for calculation.
4. If the trial mixes does not gives the required properties of the mix, it is then required to be altered accordingly. However, when the experiences grows with the particular set of

materials and site conditions very few trials will be required, and an expert of such site very rarely will be required a 2nd trial.

## **CONCLUSION**

1. For M-30 Grade concrete having same material and requirement, but without water reducer, the PPC and OPC required will be  $190/0.45 = 422\text{kg/m}^3$
2. With the use of superplasticizer the saving in cement is  $92\text{ kg/m}^3$  and water  $45\text{ lit/m}^3$  for PPC and OPC.
3. In the Fly ash concrete the saving in cement is  $163\text{ kg/m}^3$  and water  $52\text{ lit/m}^3$  including utilization of  $111\text{ kg/m}^3$  of fly ash which is a waste material.
4. If 50 million tonnes cement in making concrete uses Water Reducers 7500000 tonnes of cement can be saved. 3750000 KL of potable water will be saved and the saving of Rs. 3300 crores per year to the construction Industry. 6975000 tonnes of CO<sub>2</sub> will be prevented to be emitted to the atmosphere. The benefits in the uses of water reducers not limited to this. When water reduces shrinkage and porosity of concrete are reduced which provides the durability to concrete structures.
6. India is facing serious air, water, soil, food and noise pollution problems. Every effort therefore are necessary to prevent pollution on top priority basis.

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**Table. 1: Grading of Aggregates**

IS Sieve Designation	Percentage Passing		
	Fine Aggregate	Crushed Aggregate	
		10 mm	20 mm
40 mm	—	—	100
20 mm	—	—	100
12.5 mm	—	100	—
10 mm	100	85	4
4.75 mm	99	5	0
2.36 mm	88	0	
1.18 mm	74		
600 Micron	43		
300 Micron	24		
150 Micron	6		

**Table. 2: Approximate free-water content (kg/m<sup>3</sup>) required to give various levels of workability for non-air-entrained (with normal entrapped air) concrete.**

Maximum size of aggregate (mm)	Type of aggregate	Slump (mm)	Degree of workability	25-75	50-100	100-180
				...	...	
			— vary			

			low	Low	Medium	...
						High
10	Uncrushed Crushed		150	205	220	240
			180	235	250	265
20	Uncrushed Crushed		140	180	195	210
			170	210	225	245
40	Uncrushed Crushed		120	160	175	190
			155	190	205	220

Note:- When coarse and fine aggregate of different types are used, the free water content is estimated by the expression.

Where,  $W_f$  = Free water content appropriate to type of fine

Aggregate And  $W_c$  = Free water content appropriate to type of coarse aggregate.

**Table. 3: Proportion of fine aggregate (percent) with 10mm and 20mm maximum sizes of aggregates and with different workability**

Grading Zone of F.A	W/C Ratio	10 mm aggregate				20 mm aggregate			
		Workability				Workability			
		VL	L	M	H	VL	L	M	H
I	0.3	43-53	46-56	49-60	54-67	32-39	35-42	39-47	44-53
	0.4	46-56	48-58	51-62	57-69	34-42	37-45	41-49	46-56

	0.5	48-58	50-61	53-65	59-72	37-45	39-47	43-52	48-59
	0.6	50-61	52-63	56-68	62-75	39-47	41-50	45-54	50-61
	0.7	52-64	55-66	58-70	64-77	41-50	44-53	47-57	53-64
II	0.3	36-43	37-46	40-49	44-54	27-32	28-35	32-39	35-44
	0.4	37-46	39-48	42-51	46-57	28-34	30-37	33-41	37-46
	0.5	39-48	41-50	44-53	47-59	30-37	32-39	35-43	39-48
	0.6	41-50	42-52	45-56	49-62	32-39	34-41	36-45	41-50
	0.7	42-52	44-55	47-58	51-64	34-41	36-44	38-47	43-53
III	0.3	29-36	32-37	33-40	37-44	23-27	24-28	27-32	30-35
	0.4	31-37	33-39	35-42	38-46	24-28	26-30	28-33	31-37
	0.5	32-39	34-41	36-44	40-47	25-30	27-32	29-35	33-39
	0.6	34-41	36-42	38-45	42-49	27-32	29-34	31-36	35-41
	0.7	35-42	37-44	39-47	43-51	28-34	30-36	32-38	36-43
IV	0.3	26-29	27-32	29-33	32-37	19-23	21-24	23-27	26-30
	0.4	27-31	29-33	30-35	34-38	21-24	22-26	24-28	28-31
	0.5	28-32	30-34	32-36	35-40	22-25	24-27	26-29	29-33
	0.6	30-34	31-36	33-38	36-42	23-27	25-29	27-31	30-35

	0.7	31-35	32-37	35-39	37-43	25-28	26-30	28-32	32-36
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**Table. 4: Proportion of fine aggregate (percent) with 40 mm maximum sizes of Aggregates and with different workability.**

Grading Zone of F.A	W/C Ratio	40 mm aggregate Workability			
		VL	L	M	H
I	0.3	27-33	29-35	33-39	38-46
	0.4	29-35	31-38	35-42	41-49
	0.5	31-38	33-41	37-44	43-52
	0.6	33-41	36-43	39-47	45-54
	0.7	36-44	38-46	42-50	47-57
II	0.3	22-27	23-29	27-33	31-28
	0.4	24-29	25-31	28-35	32-41
	0.5	25-31	27-33	30-37	34-43
	0.6	27-33	29-36	32-39	36-45
	0.7	29-36	31-38	34-42	38-47
III	0.3	18-22	20-23	22-27	26-31
	0.4	20-24	21-25	24-28	27-32

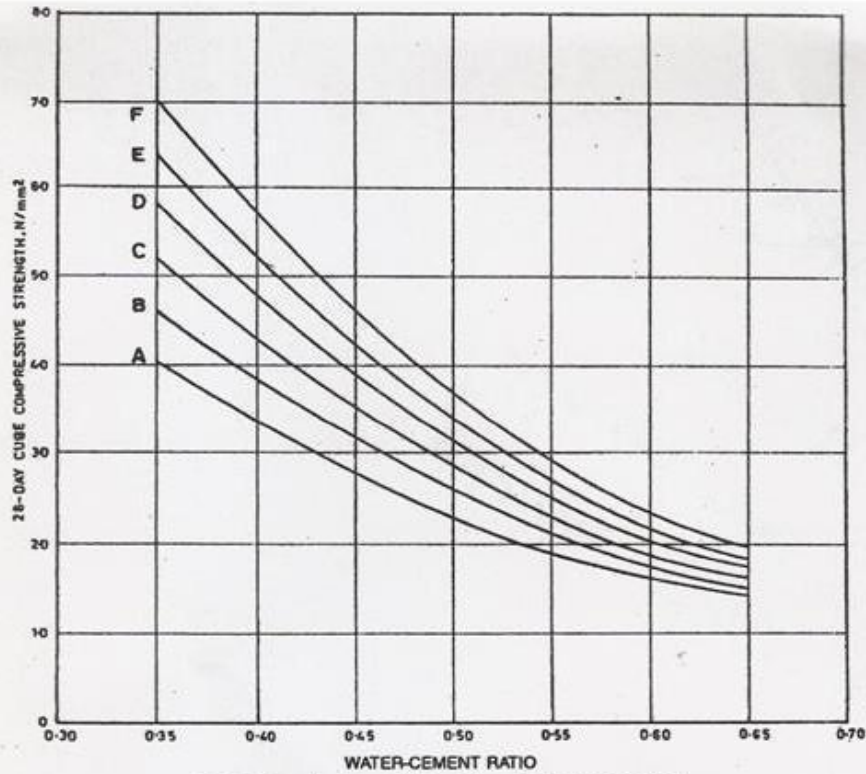
	0.5	21-25	23-27	25-30	29-34
	0.6	23-27	24-29	27-32	30-36
	0.7	24-29	26-31	29-34	32-36
IV	0.3	16-18	18-20	19-22	22-26
	0.4	17-20	19-21	20-24	24-27
	0.5	18-21	20-23	22-25	25-29
	0.6	20-23	22-24	23-27	26-30
	0.7	21-24	23-26	25-29	28-32

$V_L$  = Very low workability.

L = Low workability – slump 25-75 mm

M = medium workability – slump 50-100 mm

H = High workability- slump 100-180 mm

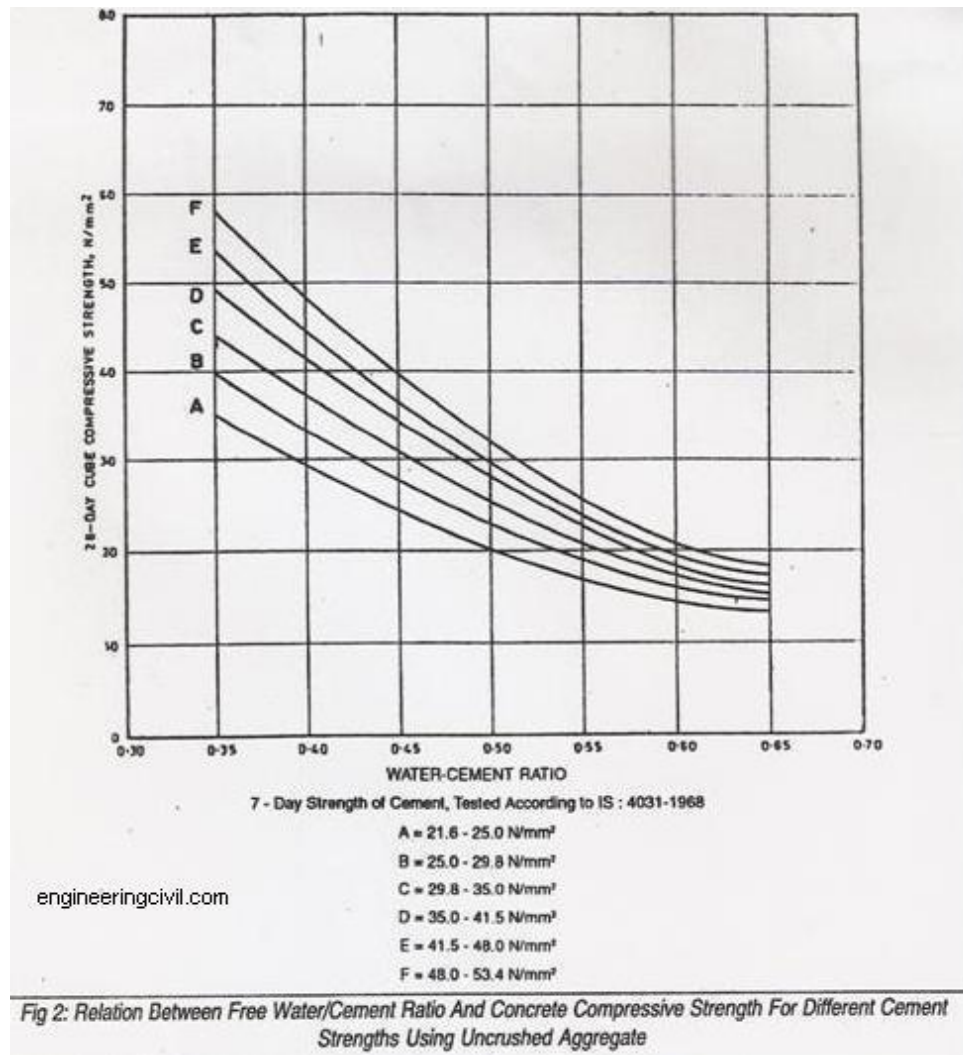


7 - Day Strength of Cement, Tested According to IS : 4031-1968

A = 21.6 - 25.0 N/mm <sup>2</sup>	D = 35.0 - 41.5 N/mm <sup>2</sup>
B = 25.0 - 29.8 N/mm <sup>2</sup>	E = 41.5 - 48.0 N/mm <sup>2</sup>
C = 29.8 - 35.0 N/mm <sup>2</sup>	F = 48.0 - 53.4 N/mm <sup>2</sup>

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Fig 1: Relation Between Free Water / Cement Ratio And Concrete Compressive Strength For Different Cement Strengths Using Crushed Aggregate



We are thankful to Sir Kaushal Kishore for publishing his unpublished research paper here on the website. This would be of great use to all the civil engineers who work are looking for some cost effective measures.

Source: <http://www.engineeringcivil.com/cement-and-water-saving-with-water-reducers.html>